WELDING INSTRUCTIONS PROTECTION 380 | 400 | 450 | 500

GENERAL WELDING INFORMATION

Miilux® Protection steel grades are manufactured by hardening, and thus attention should be paid on their heat input and pre-heating. Protection steels must be welded with filler material a with low hydrogen content. Carbon equivalent value (CEV) clearly affects the weldability of steels.

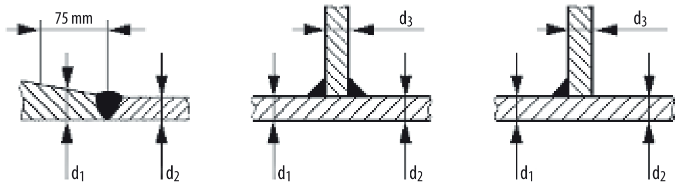
The carbon equivalent value of Protection steels is calculated using the following equation: **CeV= C+mn/6+(Cr+mo+V)/5+(ni+Cu)/15** The composition needed in order to calculate the carbon equivalent value is indicated in the manufacturer's inspection document. The higher the carbon equivalent value the easier the steel hardens and loses its tensile properties in welding.

WORKING TEMPERATURES AND HEAT INPUT

Table 1 shows the recommended working temperatures of certain heat input values Q. The pre-heating temperature of the plate must be a minimum of 70 % of the working temperature, and the temperature of the plate must not exceed the recommended working temperature by much over 30 %. Thin plates in particular tend the heat too much, which will cause Protection steels to lose their good properties.

The composition of attachments and wall thickness must be taken into account when determining pre-heating and working temperatures. Equations for combined plate thicness are shown in figure 1. The recommended heat input area for a 20 – mm plate (combined plate thickness) is 1 – 2 kJ/mm and 40-mm plate 1,5 – 2,5 kJ/mm.

Figure 1 | Calculation of joint plate thickeness



d1 = Average thickness in 75mm long section. Compined plate thickness = d1 + d2

Both sides are welded simultaneously. Combined plate thickness = 1/2 x (d1 + d2 + d3)

Combined plate thickness = d1 + d2 + d3

Table 1 | Recommended working temperatures

Steel grade	(Q kJ/ mm)	Combined plate thickness $d_1 + d_2 + d_3$		
		20 mm	30 mm	40 mm
PROTECTION 380/400	1			100 °C
PROTECTION 380/400	2			75 °C
PROTECTION 380/400	3			75 °C
PROTECTION 450	1		100 °C	125 °C
PROTECTION 450	2		100 °C	100 °C
PROTECTION 450	3		75 °C	100 °C
PROTECTION 500	1	100 °C	125 °C	150 °C
PROTECTION 500	2	100 °C	125 °C	125 °C
PROTECTION 500	3	100 °C	100 °C	125 °C

Q=(U*I*60)/(v*1000) [kj/mm]

WELDING CONDITIONS

Difficult conditions at the site, such as wind, rain or dirt, will negatively affect the quality of the weld and poor lighting will make welding more difficult. Poor welding equipment are not suitable for the welding of Protection steels: welding wire feed must work or the welding electrode must remain firmly in the welding socket. Without these factors, making a good welded joint is difficult.

It is recommended to turn the welded object to the most favourable welding position, which most often is the flat position.

GROOVE PREPARATION AND SHAPE

Cleaning the weld grooves from swarf, dirt and grease before welding is important in groove preparation. Carbon arc gouging should be avoided when manufacturing the grooves because it causes carbonisation of the melt created during gouging and its hardening properties, due to the high carbon content, may be critical. Carbon content after carbon arc gouging may be as high as double, in which case a critical zone in terms of strength and tensile properties will be created inside the weld.

The need for carbon arc gouging can be avoided by using a sufficiently large root opening (2 – 4 mm) in the groove. A smaller root opening and, for example, one-sided V-groove are sufficient when welding a thin plate. In case of joining thick and thin plates by welding, the groove should always be on the side of the thinner plate.

Fillet welds in Protection steels present a risk. The joint tends to crack under the fillet. If using a fillet weld cannot be avoided, the weld must be made as robust and solid as possible.

Good engineering must be used in order to avoid difficult corner welds in Protection. Accessibility should thus be taken into account when designing weld joints.

A groove must be finished by grinding.

SELECTION OF THE WELDING PROCESS

Heat input limits of steel grades and the method of welding must be taken into account when selecting the welding process. The impact of the selection of the welding process, welding method and welding energy is highlighted as the strength of the steel grades increases and the quality class of impact strength rises. Good impact strength in the weld can be achieved using all common welding processes (MIG/MAG, flux-cored welding, submerged arc welding, metal arc welding) provided that welding energy is maintained in compliance with the recommendations for a given steel grade.

It is recommended to use mechanical welding whenever possible, because it allows better productivity and usually also better impact strength than in manual welding.

SELECTION OF FILLER METALS

When welding Protection steels, it is often beneficial to use filler metals that are softer than the basic material and use engineering in order to avoid locating welded joints in parts that are most loaded or exposed to high stress. In addition, in the case of the highest alloyed steel grades, the mixing of basic material with the weld metal increases the strength of the weld material as much as about 100 MPa compared to the listed values for pure filler metals. It is also recommended to select low-hydrogen filler materials to keep the hydrogen level sufficiently low.

The commonly used filler metals for Protection steels are ESAB OK 48.00 and OK Autrod 12.51. If high strength in the welded state is required from the filler metal, it is recommended to use the OK 75.75 or OK Autrod 13.10/13.12 filler metals. Equivalent filler metals can also be found from other suppliers, such as Elga, Lincoln and Oerlikon.

HANDLING OF FILLER METALS

Filler metals must be dried before use to ensure that they contain no hydrogen. The producer's instructions must be followed in storing, handling and using filler metals.

WELDING ORDER AND FINISHING

When welding Protection steels, two superimposed passes must always be used. This way, the lower pass can be annealed (hardness decreases but tensile strength increases). Consecutive measures can be considered after two passes have been welded. The harder the material, the more important it is to have two superimposed passes. The last pass should be left incomplete rather than overfilled. Filling the weld transversally is not recommended under any circumstances.

Temperature control is very important in welding. Welding must be completed properly (from hefts to grinding using the same temperature), because welding on top of a cooled pass will multiply welding stress, which increases the total stress of the work. This in turn exposes the weld and the welded work to breaking in use. It must be borne in mind that every pass causes longitudinal stresses equivalent to the yield point of the material in the piece welded. Welding is completed only when the joints are filled and surfaces and corners have been round. The weld class can be defined, for example, on the basis of the SFS EN-ISO 5817 standard.

THERMAL CUTTING

Preheating and working temperatures must be adapted in thermal cutting. When using a large cutting nozzle in thermal cutting, travel speed must be proportionally greater. Travel speed is too great only when drag starts to form on the lower surface of the cut joint.

Miilux Ltd
Ruonankatu 1, 92100 Raahe, Finland
Tel. +358 10 5856 000
Fax.+358 10 5856 381
www.miilux.fi
www.miiluxprotection.fi